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Evaluation of an InAlN/AlN/GaN HEMT with Ta-based ohmic contacts and PECVD SiN passivation

Anna Malmros^{*1}, Piero Gamarra^{**2}, Mattias Thorsell¹, Marie-Antoinette di Forte-Poisson², Cedric Lacam², Maurice Tordjman², Raphaël Aubry², Herbert Zirath¹, and Niklas Rorsman¹

¹ Chalmers University of Technology, Kemiv. 9, 41296 Göteborg, Sweden

² 3-5 Lab/Thales Research & Technology, Route de Nozay, 91460 Marcoussis, France

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* Corresponding author: e-mail anna.malmros@chalmers.se, Phone: +46 (0)31 772 5049, Fax: +46 (0) 31 164513

** e-mail piero.gamarra@3-5lab.fr, Phone: +33 1 30777 148, Fax: +33 1 30776786

An InAlN/AlN/GaN HEMT with Au-free Ta-based ohmic contacts and a high-quality PECVD SiN passivation is reported. The ohmic contacts were annealed at 550 °C, resulting in a contact resistance of 0.64 Ωmm. The gate length was 50 nm. The device performance and the process were evaluated by performing DC-, pulsed IV-, RF-, and load-pull measurements. It was observed that current slump was effectively mitigated by the pas-

sivation layer. The DC channel current density increased by 71 % to 1170 mA/mm at the knee of the IV curve, and the transconductance increased from 382 to 477 mS/mm after passivation. At the same time the gate leakage increased, and the extrinsic f_{max} decreased from 207 to 140 GHz. Output powers of 4.1 and 3.5 W/mm were measured after passivation at 31 and 40 GHz, respectively.

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1 Introduction The AlGaIn/GaN HEMT has shown to be a very promising candidate for high output power and high frequency applications. One obstacle in this technology has been reliability, partly owing to the lattice mismatch between AlGaIn and GaN. InAlN on the other hand can be grown lattice matched to GaN at an In content of about 17 %. Commonly a thin AlN exclusion layer is used at the InAlN/GaN interface to decrease scattering caused by interface roughness and alloy disorder, thereby increasing the mobility [1]. The strong spontaneous polarization in this material implies a larger amount of electrons in the channel for a given thickness, as compared to AlGaIn/GaN heterostructures. Conversely, it can produce the same amount of electrons as a conventional AlGaIn/GaN heterostructure, but with a thinner barrier layer. Hence the material is of interest for both high-power [2] and high frequency applications.

Ohmic contacts are an essential part of a microwave transistor. Apart from a low contact resistance a smooth surface morphology is important for the detection of alignment marks and scaling of the drain/source-gate dis-

tance. It has been demonstrated previously that Ta/Al/Ta metallization can produce low-resistive ohmic contacts to AlGaIn/GaN when annealed at the comparatively very low temperature of 550 °C [3]. In this study we show that also InAlN/AlN/GaN HEMTs may be fabricated with Ta-based ohmic contacts. This resulted in a low contact resistance and a very smooth surface morphology. The devices were downscaled laterally and vertically in order to promote high-frequency performance. Measurements including DC, pulsed IV, RF, and load-pull at 31 and 40 GHz were performed before and after deposition of the passivation layer.

2 Fabrication The InAlN/AlN/GaN heterostructure was grown by low pressure metal-organic chemical vapor deposition (MOCVD) on 3 inch SiC substrate using a close coupled multiwafer reactor. Trimethyl gallium (TMGa), trimethyl indium (TMIn), and trimethyl aluminium (TMAI) were used as group III precursors and ammonia (NH₃) as group V precursor. The heterostructure consisted of a 100 nm high temperature AlN nucleation layer, a high resistive 1.6 μm GaN buffer layer followed by a 2 nm thick

AlN interlayer and a 6 nm undoped InAlN layer with In content of 18.8 %. At this In content, InAlN grown on GaN is nearly lattice matched. Details on the growth of nearly lattice matched InAlN/AlN/GaN HEMT structures may be found in [4].

Devices with a gate width of $2 \times 50 \mu\text{m}$ and a gate length of 50 nm were processed. Processing started with the formation of mesas in a Cl_2/Ar plasma. Ohmic contacts separated by $1 \mu\text{m}$ were defined by e-beam lithography (EBL). The contact metallization consisted of a Ta/Al/Ta stack which was annealed at 550°C in N_2 ambient. Ni/Au gates, defined with EBL using a ZEP520/UV5 resist stack [5], were centered in the drain-source opening. Definition of contact electrodes was done by optical lithography followed by deposition of Ti/Au. Finally a 250 nm thick SiN passivation layer was deposited at 340°C by PECVD.

3 Results and discussion The contact resistance was $0.64 \pm 0.03 \Omega\text{mm}$ as measured with the transmission line method (TLM). The contacts exhibited a very smooth surface morphology, Fig. 1.

IV characteristics improved considerably after passivation. The channel current density increased by 71% to 1170 mA/mm at $(V_{\text{gs}}, V_{\text{ds}}) = (1, 2.4) \text{ V}$, Fig. 2. The maximum transconductance improved from 382 to 477 mS/mm , Fig. 3. These results were consistent with Hall measurement data, showing an increase in the sheet charge density from 1.4 to $1.6 \times 10^{13} \text{ cm}^{-2}$, while the mobility dropped from 1630 to $1590 \text{ cm}^2 \cdot \text{V}^{-1} \cdot \text{s}^{-1}$. This resulted in an overall decrease in the sheet resistance from 270 to $239 \Omega/\square$. Despite the fairly thin barrier the device suffered from short channel effects, making it hard to pinch the device at high drain voltages and causing high output conductance. This phenomenon was enhanced after passivation, likely due to the increased number of electrons in the channel.

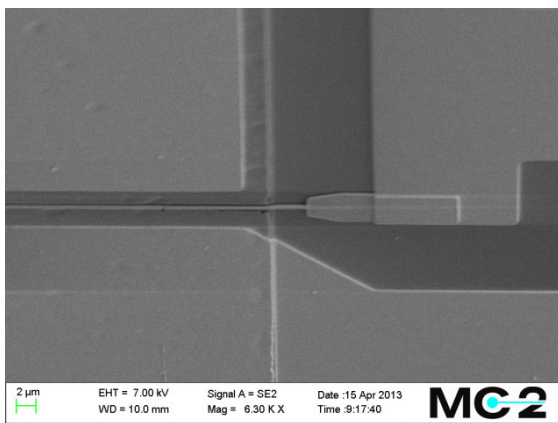


Figure 1 SEM image taken prior to passivation shows a very smooth surface morphology.

The gate leakage increased by several orders of magnitude after passivation, Fig. 4, but was still reasonably low

for a GaN HEMT ($<1 \text{ mA/mm}$). Noteworthy, the gate leakage prior to passivation was extremely low, especially considering that InAlN/AlN/GaN HEMTs are known to have problems with gate leakage. Many groups have therefore investigated MOS HEMTs as a method of suppressing gate leakage currents [6–9]. One plausible reason for the overall low gate leakage is a native oxide at the InAlN surface. The increased gate leakage after passivation may have been due to a conductive path at the InAlN/SiN interface. It is also possible that the low gate leakage prior to passivation was a result from filled surface states near the gate, depleting the channel and thereby increasing the tunneling distance. This effect would then have been mitigated by the passivation layer.

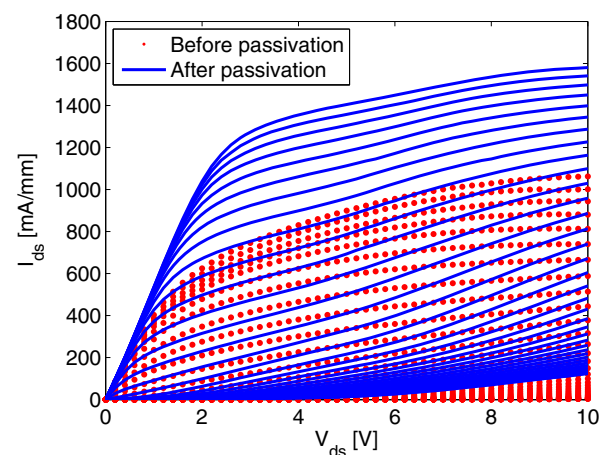


Figure 2 I_{ds} versus V_{ds} for V_{gs} ranging from -6 to 1 V with a step of 0.2 V .

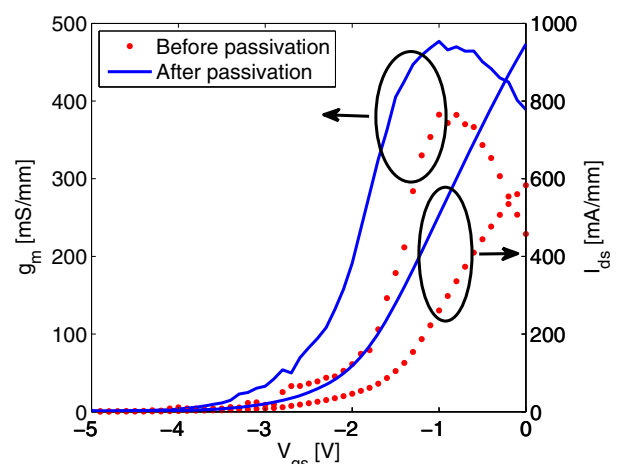


Figure 3 I_{ds} and transconductance versus V_{gs} for $V_{\text{ds}} = 3 \text{ V}$.

The presence of filled traps in the near-gate region for a negative gate bias was confirmed by pulsed IV results. The measurements were performed by applying different quiescent bias voltages ($V_{\text{gsq}}, V_{\text{dsq}}$) and thereafter pulsing to drain biases up to 9 V while the gate bias was kept con-

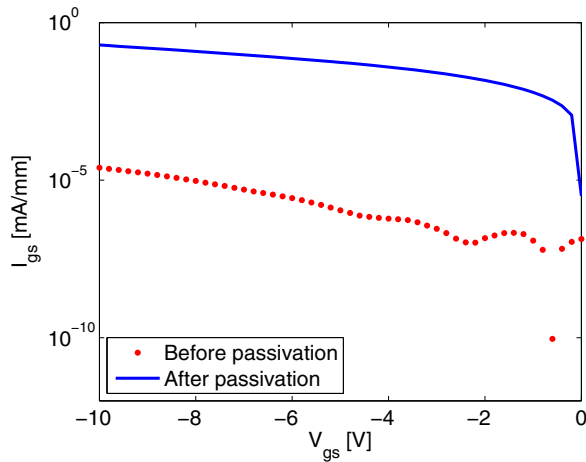


Figure 4 Gate leakage characteristics at zero drain bias.

stant a 0 V. The pulses had a duration of 0.5 μ s and were separated by 1 ms. For the unpassivated sample a large discrepancy between the output currents $I_{L_{10,10}}$ (pulsed from (-10, 10) V) and $I_{0,0}$ (pulsed from (0, 0) V) was observed, Fig. 5. This is an indication of lag effects, caused by trapped electrons at the surface and/or in the bulk. Both the on-resistance and the current in the saturated region were improved after passivation. This suggests that the majority of the electrons causing dispersive behaviour were trapped at the surface. The slump ratio, defined as $I_{L_{10,10}}/I_{0,0}$ pulsed at $V_{ds} = 3$ V improved from 12 % to 78 %.

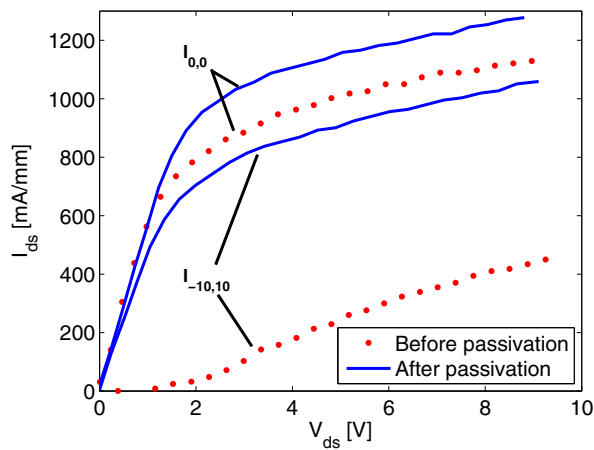


Figure 5 Pulsed IV characteristics at two different quiescent bias points.

RF measurements were performed in the 0.1 to 110 GHz range. Prior to passivation the extrinsic values of f_T and f_{max} were 90 and 207 GHz, respectively, Fig. 6a. These values were obtained by extrapolation at -20 dB/decade. f_{max} decreased considerably after passivation to 140 GHz, whereas f_T remained unchanged, Fig. 6b. The drop in f_{max} was associated with the increase in output conductance after passivation.

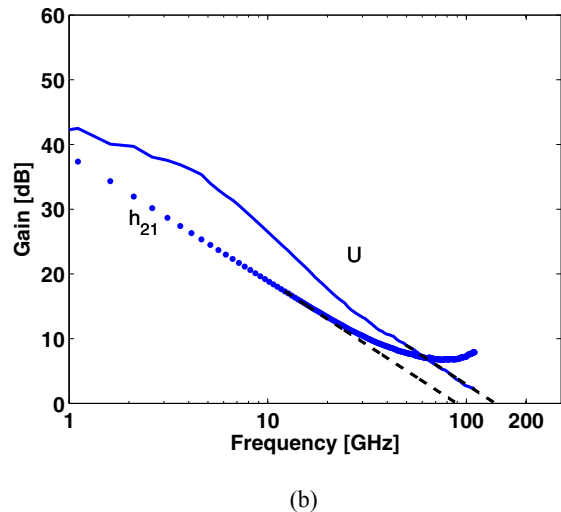
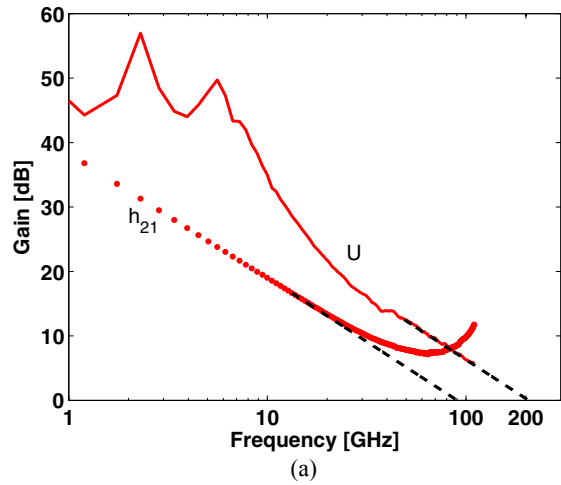


Figure 6 RF characteristics, a) before passivation and b) after passivation.

InAlN/AlN/GaN HEMTs have previously shown to deliver output powers up to 5.8 W/mm at 35 GHz [10]. In this study CW load-pull measurements were performed using a Maury system with tunable source- and load impedances. The output power was measured at 3dB gain compression, or at the maximum available input power if the 3 dB compression point was not reached. The maximum available input power was limited to 35 dBm minus the losses in the setup and reflections the inputs of the tuners.

At 31 GHz the passivated HEMT delivered a maximum output power of 4.1 W/mm and a drain efficiency of 27%, Fig. 7. The unpassivated HEMT delivered 1.7 W/mm and a drain efficiency of 19% at the same frequency. At 40 GHz the passivated and unpassivated HEMT exhibited output powers of 3.5 and 1.5 W/mm and drain efficiencies of 21 and 16%, respectively. The output power scaled with the drain bias in class A operation, Fig. 8.

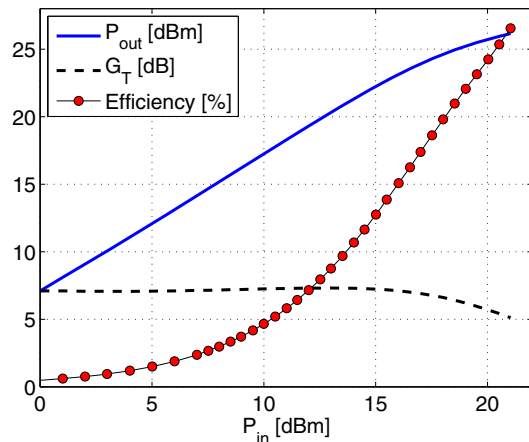


Figure 7 Results from load-pull measurements on the passivated HEMT at 31 GHz at $V_{ds} = 20$ V and $V_{gs} = -2.5$ V.

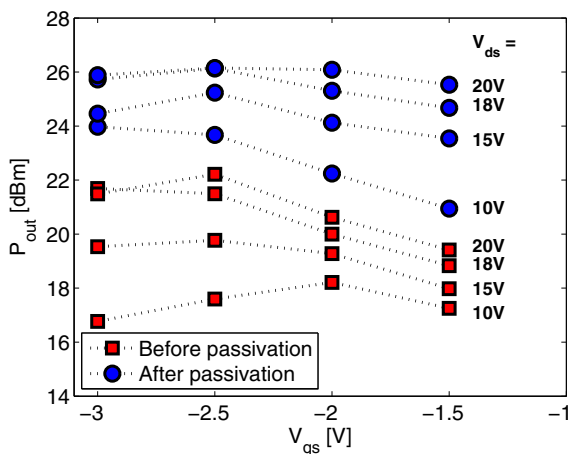


Figure 8 Output power versus bias at 31 GHz before and after passivation.

4 Conclusion An InAlN/AlN/GaN HEMT with Ta-based ohmic contacts and SiN passivation deposited by PECVD was demonstrated. The ohmic contact process yielded a contact resistance of $0.64 \Omega\text{mm}$ and a very smooth contact surface. The passivation layer effectively decreased lag effects and increased the amount of electrons in the channel. Consequently the output power increased; the maximum output power at 31 GHz was 4.1 W/mm. On the negative side the gate current increased and a considerable reduction of f_{max} was observed. Nevertheless the passivated device exhibited an extrinsic f_T and f_{max} of 90 and 140 GHz, respectively.

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