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# Improving Bandwidth Efficiency in E-Band Communication Systems

*Hani Mehrpouyan, California State University*

*M. Reza Khanzadi, Chalmers University of Technology*

*Michail Matthaiou, Queen's University Belfast*

*Akbar M. Sayeed, University of Wisconsin*

*Robert Schober, University of British Columbia*

*Yingbo Hua, University of California*

## ABSTRACT

The allocation of a large amount of bandwidth by regulating bodies in the 70/80 GHz band, that is, the E-band, has opened up new potentials and challenges for providing affordable and reliable gigabit-per-second wireless point-to-point links. This article first reviews the available bandwidth and licensing regulations in the E-band. Subsequently, different propagation models (e.g., the ITU-R and Cane models) are compared against measurement results, and it is concluded that to meet specific availability requirements, E-band wireless systems may need to be designed with larger fade margins compared to microwave systems. A similar comparison is carried out between measurements and models for oscillator phase noise. It is confirmed that phase noise characteristics, which are neglected by the models used for narrowband systems, need to be taken into account for the wideband systems deployed in the E-band. Next, a new MIMO transceiver design, termed continuous aperture phased (CAP)-MIMO, is presented. Simulations show that CAP-MIMO enables E-band systems to achieve fiber-optic-like throughputs. Finally, it is argued that full-duplex relaying can be used to greatly enhance the coverage of E-band systems without sacrificing throughput, thus facilitating their application in establishing the backhaul of heterogeneous networks.

## INTRODUCTION

The popularity of multimedia applications and broadband Internet has created an ever increasing demand for achieving higher throughputs in cellular and wireless networks. Thus far, wireless point-to-point links have played an important role in carrying a large portion of this data by interconnecting cellular base stations or enterprise buildings. In fact, due to their low cost of installation and insusceptibility to environmental effects, more than 50 percent of today's cellular

base stations are interconnected using wireless backhaul links [1]. However, if wireless point-to-point links are expected to continue to be widely applied in next generation cellular networks, they have to support throughput comparable to that of fiber optic links. This task is made difficult by the limited bandwidth available in the microwave band [2]. In this regard, the large bandwidth available in the 70 and 80 GHz or E-band has opened up new opportunities for developing multi-gigabit-per-second wireless links [1, 3].

Even though the available bandwidth in the E-band is more than 50 times the entire cellular spectrum, radio signals in the E-band are more adversely affected by environmental factors [4]. The characteristics of E-band signals and systems can be summarized as follows:

- Due to the higher carrier frequencies, the antennas are more directional, making E-band systems mainly suitable for line-of-sight (LOS) applications.

- Rain and obstacles more severely attenuate radio signals in the E-band. Consequently, with the same transmit power and link availability requirements, E-band wireless links can operate over shorter distances compared to microwave systems. For example, let us consider two point-to-point wireless systems with a 99.999 percent availability requirement and a fade margin of 0 dB: the first system, operating at 23 GHz and employing 256-quadrature amplitude modulation (QAM), can achieve a link distance of 3 km at 1.4 Gb/s, while the second system utilizing the 70/80 GHz spectrum and using binary phase shift keying (BPSK) can only operate over 1.9 km at 3 Gb/s [4].

- To achieve the high carrier frequencies required by E-band systems, a voltage controlled oscillator's signal needs to be taken to E-band carrier frequencies using a larger frequency multiplication factor compared to systems operating in the microwave band. This, in turn, can result in larger oscillator phase noise variances. Phase noise, which is present in communication systems due to imperfect oscillators, can significant-

*The ITU has allocated the 71–76 and 81–86 GHz bands for establishing wireless links throughout the world. Nevertheless, the channelization and regulations regarding the use of this spectrum differ in different regions and countries.*

ly impact their bandwidth efficiency and performance, since it results in rotation of the signal constellation from one symbol to the next symbol [5]. Moreover, in E-band systems, due to the LOS nature of the links, the coherence time of the channel is much longer than the phase noise variation time. This means that phase noise can be a performance bottleneck in E-band systems, while in other systems the channel variations might be the fundamental limitation.

- Because of the received signal's large bandwidth and high sampling rate, E-band systems require the application of high-speed digital signal processing, digital-to-analog conversion (D/A), and analog-to-digital conversion (A/D) units at the transceivers.

- Due to the very high carrier frequencies, the power amplifiers used in E-band systems have a very limited output range and are inefficient compared to those employed in the microwave band. Hence, the output power levels of most existing E-band systems are lower than the maximum levels allowed by regulating bodies. This further limits the operating range of these systems.

Because of these limitations, thus far, most E-band systems use low order modulations such as BPSK and on-off keying, and are not spectrally efficient compared to traditional microwave links. In fact, current E-band systems achieve a spectral efficiency of 0.5–2.4 b/s/Hz [6], whereas the spectral efficiencies of traditional microwave systems are in the range of 4–12 b/s/Hz [7].

To enable the development of multi-gigabit-per-second wireless links, it is paramount to introduce new transceiver designs for E-band systems that can more efficiently utilize the available bandwidth, while supporting wireless links over distances comparable to those of microwave links. To this end, this article first reviews the bandwidth allocation and licensing in the E-band. Next, unlike previous articles that did not take into account the effect of phase noise [6, 8], by comparing measurement results with the current models for signal attenuation and oscillator phase noise, it is shown that traditional models developed for the microwave band may not accurately predict these phenomena in the E-band. The development of more accurate models is anticipated to result in better link budget planning and more accurate tracking of phase noise, which can in turn enhance the bandwidth efficiency of E-band systems (e.g., enabling the application of higher order modulations). Subsequently, a new multiple-input multiple-output (MIMO) transceiver design, termed continuous aperture phased MIMO (CAP-MIMO), is outlined, and new topologies and applications for E-band systems are proposed that can mitigate their limitations and better utilize their potential.

The remainder of this article is organized as follows. The available bandwidth in and the regulations on the E-band are summarized. We focus on the models for channel attenuation and oscillator phase noise for the E-band. The CAP-MIMO transceiver design for E-band systems is presented, and we then propose new topologies and applications for E-band systems.

## BANDWIDTH AND LICENSING IN THE E-BAND

The International Telecommunication Union (ITU) has allocated the 71–76 and 81–86 GHz bands for establishing wireless links throughout the world. Nevertheless, the channelization and regulations regarding the use of this spectrum differ in different regions and countries.

### UNITED STATES

In the United States, the entire 10 GHz of bandwidth in the 71–76 and 81–86 GHz bands is available for utilization without any specific sub-channelization. This approach provides a great potential for deployment of very high-speed frequency-division duplex (FDD) wireless links. In addition, the Federal Communications Commission (FCC) set the effective isotropic radiated power (EIRP), maximum transmit power, minimum antenna gain, and maximum out of band emissions for E-band systems to 55 dBW, 35 dBm, 43 dBi, and –13 dBm, respectively. More important, due to the very high carrier frequencies and the requirement for high antenna directivity, wireless links in the E-band can be deployed in close vicinity of one another with limited interference. Therefore, the FCC has adopted a unique licensing approach for spectrum allocation in the E-band, where the links can be quickly and economically registered over the Internet.

### EUROPE

In Europe, the Conference of European Postal and Telecommunications has taken a different approach and divided the 10 GHz of spectrum in the 70/80 GHz bands into 250 MHz channels with a guard band of 125 MHz at the top and bottom end of each band. Thus, each 5 GHz band consists of 19 channels that can be used for both FDD and time-division duplex operation. Moreover, the regulations in the E-band in Europe are more stringent than the FCC rules. Specifically, in Europe the EIRP, maximum transmit power, minimum antenna gain, and maximum out of band emissions are set to 55 dBW, 30 dBm, 38 dBi, and –30 dBm, respectively, where the EIRP and maximum transmit power are also functions of the antenna gain, and are expected to be lowered as the antenna gain increases.

### ASIA

The 70/80 GHz bands are under consideration for licensing in Japan, China, and most other Asian countries, and are not yet available for commercial use.

## CHANNEL AND PHASE NOISE MODELS FOR THE E-BAND

Accurate channel and oscillator phase noise models for the E-band spectrum are essential for link budget planning and accurate tracking of phase noise in E-band systems. Both of these improvements are expected to enhance the bandwidth efficiency of E-band systems in the near

future [7]. Thus, in this section, we examine the accuracy of the existing models for both phenomena in the E-band.

### CHANNEL AND PROPAGATION CHARACTERISTICS IN E-BAND

To accurately predict the effect of environmental conditions on the performance of wireless communication systems, the ITU Radiocommunication Standards Sector (ITU-R) and Crane models have been extensively applied for link-budget planning in the microwave band. In order to determine the accuracy of these models in predicting rain intensity and the resulting signal attenuation in the E-band, a long-term measurement campaign was carried out in Gothenburg, Sweden, by Ericsson Research, where the rain intensity and signal attenuation of an E-band system were measured over a period of nine months [9]. The results of this measurement campaign and a comparison with respect to both the ITU-R and Crane models are plotted in Fig. 1. It can be observed that both the ITU-R and Crane models can rather sufficiently predict the rain intensity in this region, since the signal attenuation calculated based on the measured rain intensity is close to that of the ITU-R and Crane models. However, the measurement results in Fig. 1 show that the measured signal attenuation in the E-band is considerably higher than the attenuation predicted by both the ITU-R and Crane models. This demonstrates that both models, which are well suited for the microwave band, are not capable of accurately predicting the channel attenuation in the E-band. Thus, for E-band wireless point-to-point links to meet the expected 99.999 percent availability requirements, the fade margin needs to be chosen larger than the values calculated using the Crane and ITU-R models (e.g., 5–10 dB higher, as shown in Fig. 1). This new finding indicates that to avoid larger than necessary fade margins, more accurate channel attenuation models have to be developed for the E-band. These more accurate channel and propagation models are also anticipated to enhance the bandwidth efficiency of E-band systems.

Note that although the shortcomings of the ITU-R model in predicting the attenuation for E-band systems have also been confirmed in [8], in this work, for the first time, we present a comparison with respect to the Crane attenuation model, which is more extensively applied in North America.<sup>1</sup>

### PHASE NOISE MODELS IN E-BAND

One of the main challenges in E-band communication systems is to equip the transceivers with low-phase-noise high-frequency oscillators. Nevertheless, recent studies have shown that such oscillators may be designed using Gallium-Nitride technology, waveguide theory, and optoelectronic techniques [10, 11]. Generally, two methods are proposed to generate high-frequency oscillation [10, 11]. One is to design an on-chip high-frequency oscillator, and the other is to increase the frequency of a low-frequency oscillator by means of frequency multipliers. Even though the former is expected to result in

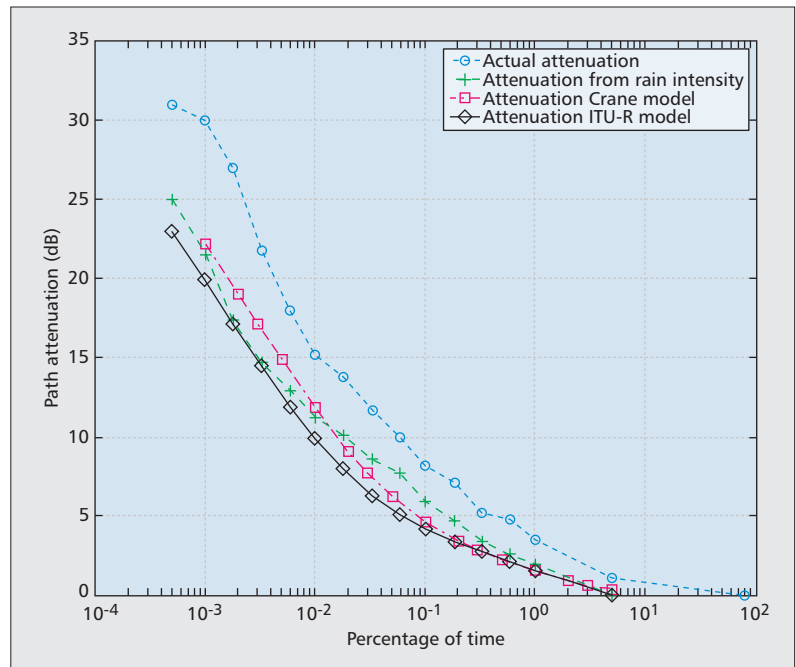


Figure 1. Path attenuation versus time with transmit power = 18.6 dBm, receiver threshold = -58 dBm, antenna gain = 43 dBi, Tx/Rx separation = 1 km 50 m, data rate = 1.25 Gb/s, differential BPSK (the measurements are also reported in [9]).

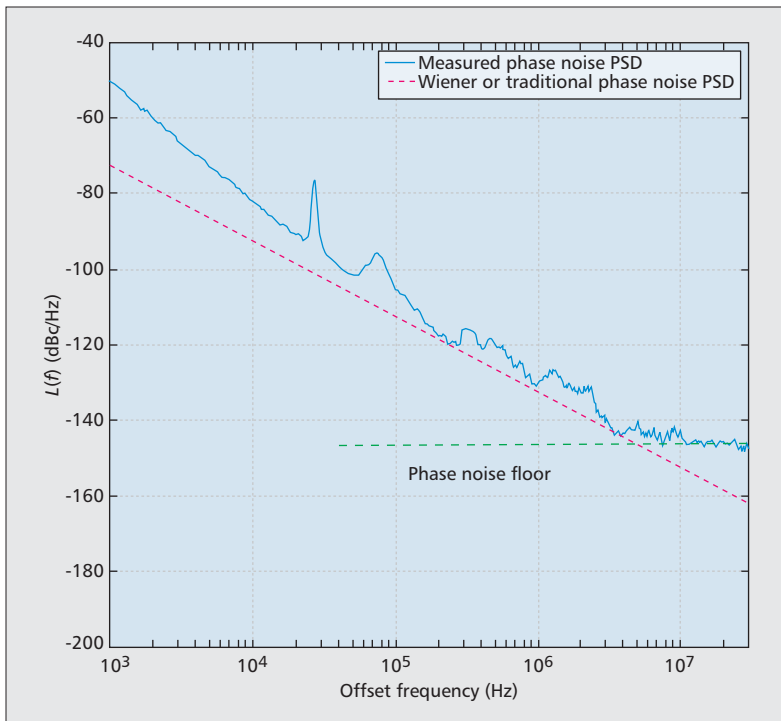
more accurate oscillators, research has shown that the design of accurate and affordable oscillators for commercial applications via this approach is a challenging task. On the other hand, the latter approach increases a low-frequency oscillator's phase noise variance by the so-called multiplication factor [10]. As a result, oscillator phase noise is one of the main limiting factors in the application of higher-order modulations in E-band systems [4].

Although the effect of oscillator phase noise in narrowband systems has been extensively studied, there is a lack of understanding of this impairment for the wideband systems deployed in the E-band. According to traditional phase noise models, the phase noise variance or rate is linearly proportional to the sampling time applied at the receiver [5]. Therefore, it is expected that systems employing larger bandwidths and smaller sampling times will experience a smaller phase noise variance. However, by increasing the signal bandwidth, other system parameters such as the bandwidth of the receiver front-end filter must also be increased. Consequently, this leads to an increase in phase perturbation introduced to the entire communication system.

To illustrate this effect in wideband systems, Fig. 2 depicts the measured power spectral density (PSD) of oscillator phase noise for a monolithic microwave integrated circuit oscillator operating at 9.9 GHz. Figure 2 compares measurement results with the traditional Wiener phase noise model, which is extensively used in the microwave band. Note that unlike the traditional phase noise models, the phase noise PSD of an oscillator does not continue to decrease with increasing offset frequency. In fact, as

<sup>1</sup> The work in [8] also provides a more accurate model compared to the ITU-R model for characterizing the channel and propagation characteristics of wireless communication systems in the E-band.

## MIMO TRANSCEIVER DESIGN FOR E-BAND SYSTEMS



**Figure 2.** The power spectral density of a free-running oscillator operating at 9.9 GHz.

shown in Fig. 2, in practice, the phase noise PSD exhibits a floor region beyond a certain offset frequency.<sup>2</sup> Thus, as the bandwidth of a communication system increases, the floor region in the PSD of an oscillator is expected to play an important role in the overall system's performance. To verify this finding, in Fig. 3, the performance of two communication systems with different bandwidths are compared in terms of the error vector magnitude (EVM) (also known as receive constellation error) for different phase noise floor levels (signal-to-noise ratio [SNR] = 30 dB and 16-QAM). Figure 3 shows that below a certain noise floor level, the cumulative phase noise is dominant, and a system with higher symbol rate experiences a lower EVM. However, as the phase noise floor increases, the performance of a communication system employing a larger bandwidth degrades more dramatically. It is also important to consider that due to the use of frequency multipliers, it is expected that most oscillators used in E-band systems have higher phase noise floor levels. For example, if the above 9.9 GHz oscillator is used in an E-band system operating at 70 GHz, a frequency multiplier with a multiplication factor of 7 needs to be applied, which will increase the noise floor by  $20\log 7 = 16.9$  dBc. Therefore, from the results in Figs. 2 and 3, it can be concluded that the phase noise models that are used for narrowband systems (e.g., the Wiener model) cannot be applied to accurately predict the properties of this impairment in wideband systems. Thus, more accurate phase noise models for wideband communication systems have to be developed to estimate and compensate for the effect of phase noise more effectively, which in turn enables the use of more bandwidth-efficient modulation schemes.

<sup>2</sup> This effect is not exclusive to this oscillator and is also reported in [5, references therein].

The development of MIMO technology has largely been based on the assumption of rich multipath, which, combined with the deployment of multiple antennas, results in multiple independent spatial channels between two terminals. Under these circumstances, it has been theoretically shown that the MIMO system capacity scales linearly with the minimum number of transmit and receive antennas. However, E-band systems are expected to operate under strong LOS conditions, thereby creating several research challenges and opportunities for the design of efficient E-band MIMO transceivers [3, 12, 13]. The antenna properties in the E-band are attractive for three important reasons:

- They result in high antenna gains for a given antenna size.
- They enable highly directional communication with narrow beams, thus reducing interference.
- They support the deployment of large-dimensional MIMO systems with relatively compact antenna arrays.

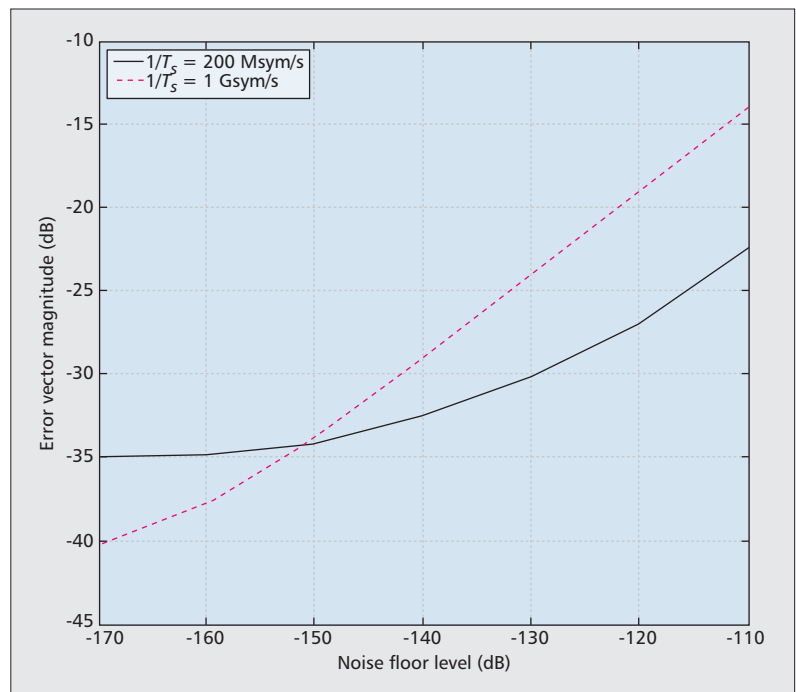
Two benchmark E-band systems dominate the current state of the art. In the first configuration, a *DISH* system, conventional continuous aperture “dish” antennas are used in highly directional LOS point-to-point links. Such systems are currently used for wireless backhaul links, for example, in the commercial systems offered by Siklu, E-band Communications, and Bridgewater. In the second configuration, *conventional MIMO*, the antenna elements are placed sufficiently far apart that the spatial LOS responses become independent. The required antenna spacing can be worked out via simple geometrical arguments and leads to the so-called Rayleigh spacing. For a given transmitter-receiver distance, the Rayleigh antenna spacing is inversely proportional to the carrier frequency. Thus, compared to microwave systems, LOS MIMO technology is more suitable for E-band systems, since the antenna spacing is smaller and the transceivers can be housed within a relatively compact module. However, while such systems can exploit multiplexing gains, they suffer from poor power efficiency and increased interference [12]. In principle, the above limitations of conventional MIMO systems can be eliminated by using half-wavelength spaced large antenna arrays. Although such systems can optimally exploit the spatial dimension, they suffer from prohibitively high transceiver complexity due to the requirement of a large number of array elements. For example, a 6” planar array operating at 80 GHz requires about 6400 antenna elements, while each antenna element requires a dedicated transceiver module [12].

Recall that propagation in the E-band is expected to have sparse multipath components and is predominantly LOS. Thus, the spatial multiplexing gain of a MIMO E-band system can, in practice, be much smaller than the minimum number of transmit and receive antennas employed. In other words, compared to a system in the microwave band, the spatial communica-

tion subspace for a MIMO E-band system can be expressed with a smaller number of orthogonal basis functions [3, 12]. Accordingly, to fully exploit the potential of MIMO technology and reduce the transceiver complexity, the number of beams transmitted or received by a MIMO E-band system needs to be equal to the dimensionality of the E-band channel subspace. This characteristic of E-band channels has motivated the development of the *CAP-MIMO* transceiver.

CAP-MIMO combines the multiplexing gain of MIMO systems, the antenna gain of DISH systems, and the beamforming capability of phased arrays to optimally exploit the smaller spatial dimensionality at E-band frequencies [12]. CAP-MIMO uses a high-resolution discrete lens array to perform analog beamforming in the passband (Fig. 4). Essentially, in this setup, a relatively small number of active beams are radiated by the corresponding feed antennas on the focal surface of the lens array. The number of transmitted beams is directly proportional to the dimensionality of the communication channel. This approach ensures that the CAP-MIMO transceiver is equipped with the smallest number of A/D, D/A, and radio frequency units, while fully taking advantage of the potential of MIMO technology. Figure 4 depicts the radio unit for a CAP-MIMO system. In this setup, it is assumed that five spatially independent channels can be established between transmitter and receiver. Consequently, the CAP-MIMO system only requires five transceiver blocks. The beam selector block in Fig. 4 ensures that appropriate beams are selected for signal transmission and reception, which is analogous to an antenna selection block in a conventional MIMO system.

Figure 5 compares the bandwidth efficiency of CAP-MIMO with a conventional MIMO system with widely spaced antennas, and a DISH system for a point-to-point LOS link at 80 GHz. The link length is about 200 m. The antenna size for the DISH and CAP-MIMO systems is 0.6 m × 0.6 m with an antenna gain of 55 dBi. The conventional MIMO system has 4 widely spaced antennas at each end, where each antenna has a gain of 30 dBi. The CAP-MIMO system is assumed to take advantage of 4 transmit and receive beams. One important observation is that the DISH system is optimum at low SNRs, whereas conventional MIMO outperforms DISH at high SNRs. CAP-MIMO yields the best performance across the entire SNR range, thereby representing a robust scheme for realizing the advantages offered in the E-band. CAP-MIMO can achieve a spectral efficiency of 30 b/s/Hz, at a normalized SNR of -8 dB with an SNR gain of about 25 dB, over the other two systems. This results in a data rate of 30–300 Gb/s for a bandwidth of 1–10 GHz. For the given antenna size, a system operating in the 3 GHz band (i.e., the microwave band, at best achieves a spectral efficiency of 10 b/s/Hz at a much higher SNR of 40 dB. This corresponds to a maximum data rate of 5 Gb/s when considering a generous bandwidth of 500 MHz. Finally, CAP-MIMO also offers a promising route to electronic multi-beamforming and steering, which can be exploited for a number of attractive operational functions, such as user tracking in mobile environments, multi-



**Figure 3.** EVM of residual phase noise error for two systems with different symbol rates vs. oscillator phase noise floor power.

beam steering in point-to-multipoint links, and formation of high-capacity cooperative MIMO links (discussed later in this article).

It is important to note that although the use of multi-antenna arrays in E-band systems has been studied [6], they are only used for power combining and not MIMO spatial multiplexing gain. As such, the CAP-MIMO concept presented here promises to provide spectral efficiencies that are significantly higher than the approach in [6] (e.g., 30 b/s/Hz for CAP-MIMO compared to 4.8 b/s/Hz for the approach in [6]). Moreover, this article uniquely provides a comprehensive comparison between the throughput of traditional MIMO and DISH systems at different SNRs.

## E-BAND POINT-TO-POINT SYSTEMS IN NEXT GENERATION CELLULAR NETWORKS

With respect to point-to-point wireless links such as backhaul links, the most important issues for cellular providers are range, very high link availability, and operating costs. To facilitate the application of E-band systems in next generation cellular networks, we propose to employ full-duplex relaying to extend the range of E-band links. Moreover, the challenges and potentials for applying E-band systems for backhauling in heterogeneous networks (HetNets) are presented.

### FULL-DUPLEX MULTIHOP COOPERATIVE RELAY NETWORKS

The research in the field of cooperative relay networks has shown that such systems can significantly enhance the coverage area and reliability of point-to-point wireless links [14]. Regenerative

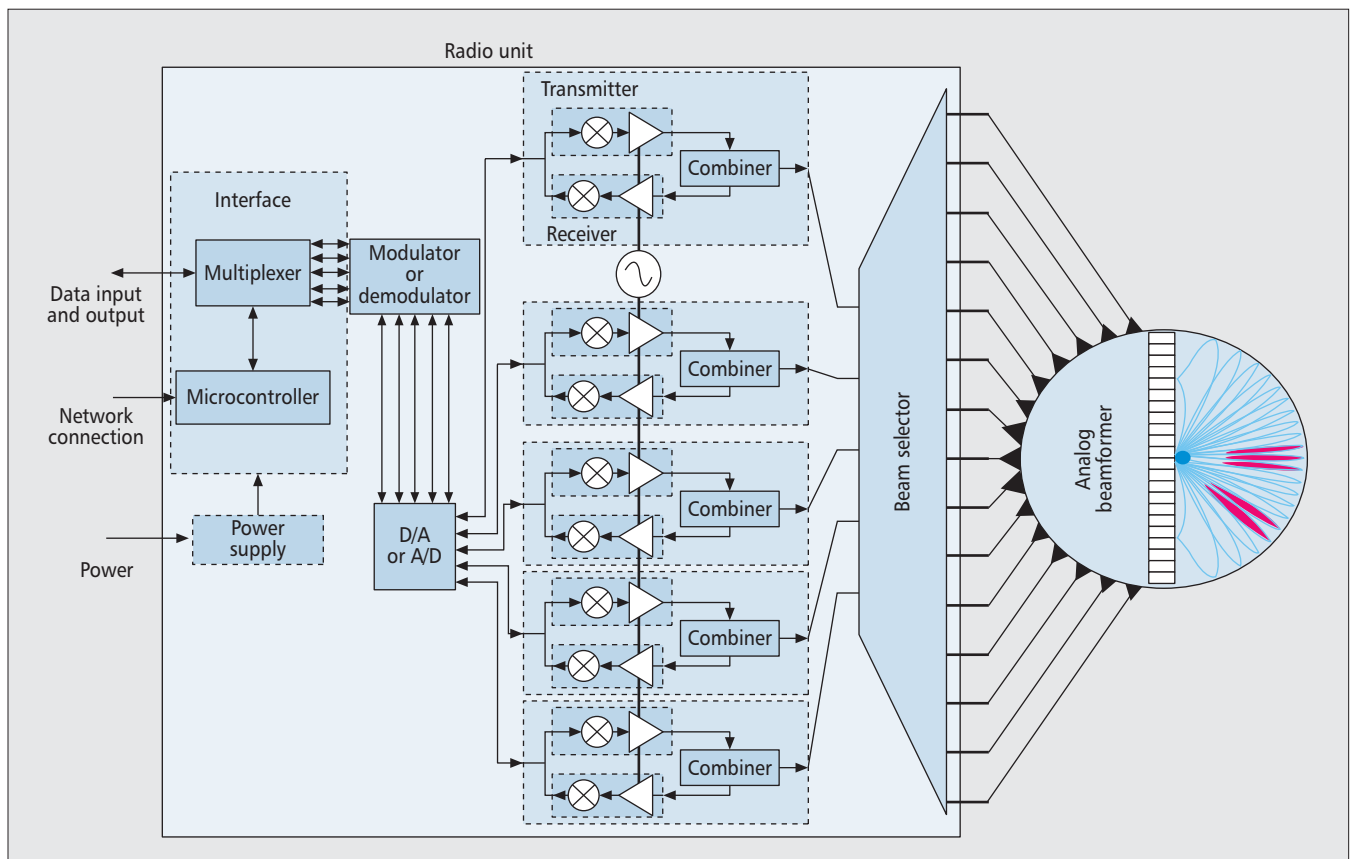


Figure 4. Radio unit for an E-band CAP-MIMO system.

and non-regenerative relaying, that is, decode-and-forward (DF) and amplify-and-forward (AF) relaying, respectively, have gained significant traction due to their performance and simplicity. However, most of the research in this area has focused on half-duplex cooperative relaying, where one node transmits while the remaining nodes stay silent. This approach reduces the throughput of the network for every additional hop. Moreover, although full-duplex relaying circumvents the shortcomings of half-duplex relaying, its implementation in the microwave band has been a challenging task. One approach is for the relays to transmit and receive at different frequency bands. However, such an approach is bandwidth inefficient and halves the potential system capacity for each additional hop. Another approach is to ensure that each node transmits and receives simultaneously over the same bandwidth. However, this scheme can result in significant interference at the relay transceiver, which degrades system performance.

Recall that E-band systems employ highly directional antennas. Thus, unlike traditional microwave systems, E-band transceiver modules can operate simultaneously without significant interference. Moreover, due to the LOS nature of E-band links and higher atmospheric absorption, E-band wireless devices can be deployed in close vicinity of one another while maintaining a low level of interference (i.e., higher spatial reuse factor). These are essential features that can enable the development of full-duplex multi-relay cooper-

ative networks in the E-band. Without sacrificing throughput, such networks can greatly enhance the range of E-band point-to-point links (Fig. 6). Moreover, AF relaying is especially attractive for full-duplex networks, since the relays may not be required to convert the signal into the baseband, thus significantly simplifying the relays' structures and reducing their hardware costs. For example, the scenario in Fig. 6 shows that by applying appropriate beamforming schemes at the transmitter and relays, the throughput of an E-band point-to-point system can be tripled, while the link distance can be doubled.

#### E-BAND SYSTEMS IN HETEROGENEOUS NETWORKS

To meet the surge in the number of users and each user's throughput requirements, cellular providers have resorted to increasing the number and density of macrocell base stations (BSs). However, as these throughput demands continue to grow, large BSs cannot effectively meet users' needs in different settings (e.g., in indoor environments and at the cell edges) [15]. Moreover, macrocell BSs are expensive to deploy and maintain. Thus, next generation cellular networks are expected to adopt the HetNet paradigm, where smaller and more specialized cells are deployed by operators, such as picocells in urban areas and femtocells in indoor environments [15]. Furthermore, to mitigate interference, achieve smooth handoffs from tier to tier, and enable

cooperation among different tiers, fast backhaul links are of paramount importance.

Since picocells and femtocells have smaller coverage areas, they can be deployed more densely throughout a cellular network. Moreover, E-band systems are capable of establishing multi-gigabit-per-second wireless links over short distances. Thus, they are well suited for establishing backhaul links among different tiers within a cell. Due to the high atmospheric absorption and the use of highly directional antennas, they can do so without causing significant interference.

There are, however, some challenges that need to be addressed. Most femtocells are expected to be deployed in indoor environments. Since E-band radio signals do not penetrate obstacles and buildings very well, E-band backhaul links may require the application of strategically positioned relays throughout the network to establish reliable connectivity between femtocell and macro-cell BSs. Another challenging issue is the high development cost of E-band transceivers. This is especially important for the development of next generation HetNets, since femtocell and picocell BSs are expected to be relatively inexpensive to manufacture. Nevertheless, recent research in the field of semiconductor design and fabrication (e.g., Silicon-Germanium and Gallium-Nitride) is expected to reduce the manufacturing costs of E-band systems and facilitate their adoption [4].

## SUMMARY

In this article, to gain a better understanding of the effects of channel attenuation and phase noise on E-band systems, measurement results for both phenomena are compared against existing models. It is concluded that the ITU-R and Cane models may not be able to accurately determine the fade margin for E-band systems; for example, if these models are used to obtain the required fade margin for an E-band link with 99.999 percent availability, the result may be 5–10 dB below the actual required value. These measurements also indicate that the floor in the PSD of oscillator phase noise may more significantly influence the performance of wideband systems operating in the E-band more than it does that of narrowband systems in the microwave band. Further research in this field is anticipated to result in E-band transceivers that can employ higher-order modulations and improved bandwidth efficiency. Next, we show that the CAP-MIMO transceiver design can enable E-band systems to achieve bandwidth efficiencies of up to 30 b/s/Hz (data rates of up to 300 Gb/s). Finally, it was proposed that due to application of highly directional antennas and the LOS nature of E-band links, full-duplex relaying can be used to extend the range of E-band systems and facilitate their application in next generation heterogeneous cellular networks.

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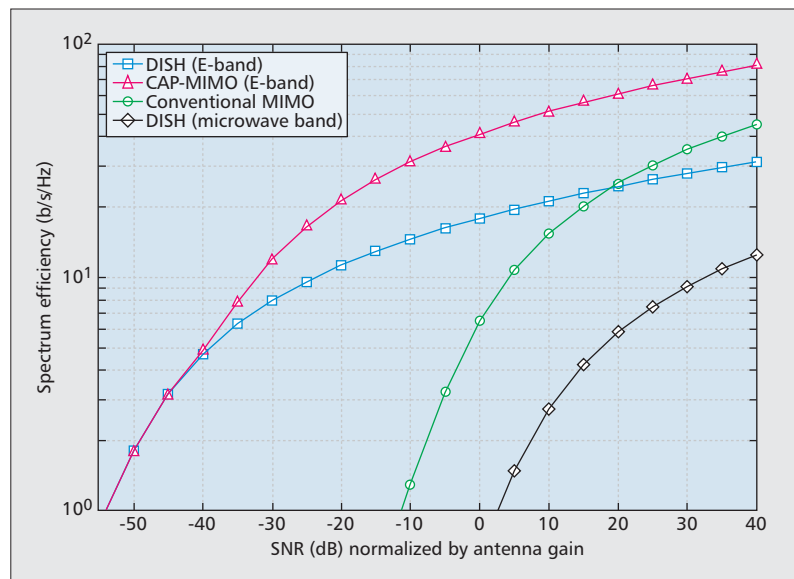


Figure 5. Bandwidth efficiency comparison of CAP-MIMO, conventional MIMO, and DISH systems.

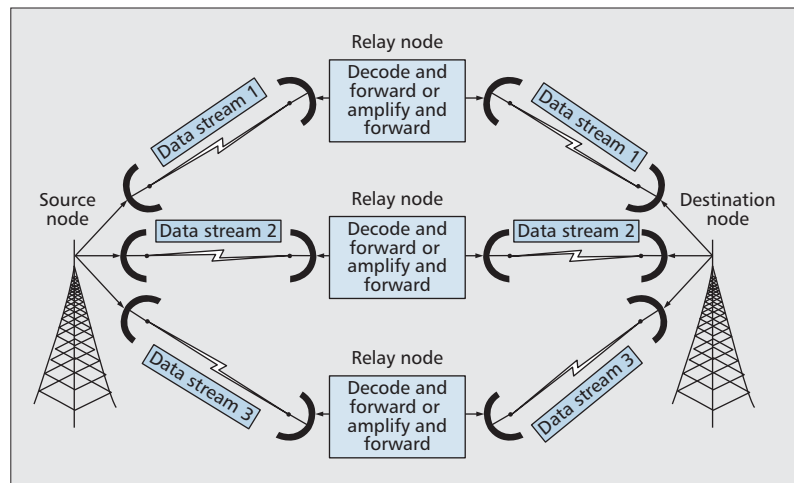


Figure 6. A full-duplex cooperative relay network in the E-band.

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## BIOGRAPHIES

HANI MEHRPOUYAN [S'05, M'10] (hani.mehr@ieee.org) received his B.Sc. honours degree in computer engineering from Simon Fraser University, Canada, in 2004 and his Ph.D. degree in electrical engineering from Queen's University, Canada in 2010. From 2010 to 2012 he was a postdoctoral researcher with the Department of Signal and Systems of Chalmers University of Technology, where he led the MIMO aspects of the microwave backhauling for next generation wireless networks project. He was also a visiting scholar at the University of Luxembourg in 2012, where he was involved in research related to interference cancellation for next generation satellite communication links. Since August of 2012 he has been an assistant professor in the Department of Computer and Electrical Engineering at California State University, Bakersfield. He has received more than 10 scholarships and awards. He has more than 30 publications in prestigious IEEE journals and conference proceedings. He has also been involved with industry leaders such as Ericsson AB, Research in Motion (RIM), and Alcatel. His current research interests lie in the area of applied signal processing and the physical layer of millimeter-wave communication systems, synchronization, channel estimation, interference cancellation, and performance optimization. For more information refer to [www.mehrpouyan.info](http://www.mehrpouyan.info).

M. REZA KHANZADI [S'10] (khanzadi@chalmers.se) received his M.Sc. degree in communication engineering from Chalmers University of Technology, Gothenburg, Sweden, in 2010. He is currently a Ph.D. candidate in the Department of Signals and Systems of the same university. He was the recipient of the S2 Pedagogical Prize 2012 from Department of Signals and Systems, as well as a 2013 Ericsson's Research Foundation grant. Bayesian inference, statistical signal processing, and information theory are his current research interests.

MICHAIL MATTHAIIOU [SM] (michail.matthaiou@chalmers.se) is currently a senior lecturer at Queen's University Belfast, United Kingdom, and holds an adjunct assistant professor at Chalmers University of Technology. He received his Ph.D. from the University of Edinburgh, United Kingdom, in 2008. He was the recipient of the 2011 IEEE ComSoc Young Researcher Award for the Europe, Middle East and Africa Region. He currently serves as an Associate Editor for *IEEE Transactions on Communications* and *IEEE Communications Letters*.

AKBAR M. SAYEED [F] (akbar@engr.wisc.edu) is a professor of electrical and computer engineering at the University of Wisconsin-Madison. He received his B.S. degree from the University of Wisconsin-Madison in 1991, and his M.S. and Ph.D. degrees from the University of Illinois at Urbana-Champaign in 1993 and 1996, all in electrical and computer engineering. He was a postdoctoral fellow at Rice University from 1996 to 1997. His research interests include wireless communications, statistical signal processing, multi-dimensional communication theory, time-frequency analysis, information theory, and applications in wireless communication and sensor networks. He was a recipient of the Robert T. Chien Memorial Award (1996) for his doctoral work at Illinois, the NSF CAREER Award (1999), the ONR Young Investigator Award (2001), and the UW Grainger Junior Faculty Fellowship (2003). He has served the IEEE in a number of capacities, including as a member of the Signal Processing for Communications and Networking Technical Committee of the IEEE Signal Processing Society (2007–2012) and an Associate Editor for *IEEE Transactions on Signal Processing* (2013–).

ROBERT SCHÖBER [S'98, M'01, SM'08, F'10] (rschober@ece.ubc.ca) received his Diplom (Univ.) and Ph.D. degrees in electrical engineering from the University of Erlangen-Nürnberg, Germany, in 1997 and 2000, respectively. From May 2001 to April 2002 he was a postdoctoral fellow at the University of Toronto, Canada. Since May 2002 he has been with the University of British Columbia, Canada. Since January 2012 he has been Alexander von Humboldt Professor and Chair for Digital Communication at the Friedrich Alexander University (FAU), Erlangen, Germany. His research interests are in the areas of communication theory, wireless communications, and statistical signal processing. He received the 2002 Heinz Maier-Leibnitz Award, the 2006 UBC Killam Research Prize, the 2007 Wilhelm Friedrich Bessel Research Award, the 2008 Charles McDowell Award for Excellence in Research from UBC, a 2011 Alexander von Humboldt Professorship, and a 2012 NSERC E.W.R. Steacie Fellowship. Moreover, he received best paper awards from the German Information Technology Society (ITG), IEEE WCNC 2012, IEEE GLOBECOM 2011, and IEEE ICUBW 2006. He is a Fellow of the Canadian Academy of Engineering and the Engineering Institute of Canada. He is currently Editor-in-Chief of *IEEE Transactions on Communications*.

YINGBO HUA [S'86, M'88, SM'92, F'02] (yhua@ee.ucr.edu) received his B.S. degree (1982) from Southeast University, Nanjing, China, and his M.S. (1983) and Ph.D. degrees (1988) from Syracuse University, New York. He held faculty positions with the University of Melbourne in Australia during 1990–2001. He was on leave at Hong Kong University of Science and Technology in 1999–2000, and consulting with Microsoft Research, Washington, in summer 2000. He has been a professor with the University of California at Riverside since 2001. His interests span the fields of sensing, signal processing, and communications, where he has published hundreds of papers with more than 6000 citations. He was elected as a Fellow of AAAS in 2011.